

https://doi.org/10.26637/MJM0S01/08

Performance analysis of a juice packaging plant using BFT

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Abstract

In this paper we are analyzing the performance of a juice packaging plant by finding various reliability parameters. The juice plant under consideration consists of a total of 11 components/ subsystems operating. According to working of them, a mathematical model has been developed and using Boolean function technique (BFT) expressions for various reliability parameters are obtained. At last a numerical example is included to study effect of various failures over the performance of the system.

Keywords

SVT, RPT, BFT, Series and Parallel configuration, Reliability and MTTF.

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Article History: Received 24 December 2017 ; Accepted 21 January 2018

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1. Introduction

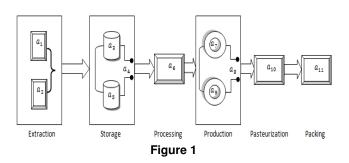
With the development of technology and modernization of our society juice manufacturing and packaging business has attracted various industries and now a days so many companies are in this business of juice packaging. At present customers are having options of selecting best of available brands which is due to the reliability created by their product quality as well as availability and cost of the product. So each company wants to improve the performance of their plant.

There are so many techniques available to solve mathematical model such as supplementary variable technique (SVT), Regenerative point technique (RPT) and Boolean function technique (BFT) etc. [8] use supplementary variable to find out various reliability parameters of a three state repairable system, [9,11,12] used Boolean function technique in their papers to obtain expressions for various reliability parameters. [5] in his work discus the working of a juice plant and explain various stages involved in the juice packaging process. Keeping all these in view the authors has taken the problem of juice packaging plant and developed a mathematical model of same which consists of a total of 11 components/ subsystems operating. According to working of them, a mathematical model has been developed Boolean function technique (BFT) has been used to solve the model. Expression for Reliability and MTTF are obtained. At last a numerical example is included to study effect of components working over the performance of the system.

There are 11 components/ subsystems denoted by a_i , where $i = 1, 2, 3, \dots, 11$ in the juice packaging plant under consideration. The raw fruits are used in extraction section which consists of two extractor units a_1 , a_2 to extract juice. Juice is stored in two storage tanks a_3 , a_5 which are in standby arrangement with perfect switching a_4 . When a_3 is not in action, identical unit a_5 start to operate. Now juice is pumped forward in Processing unit a_6 for heat treatment and refining. Now the juice can be used to produce different variety as per its utility like ready to drink juice (RTD), concentrated juice. So in production section (a_7, a_9) , the unit a_7 operate for blending and formulation of ready to drink juice (RTD) and unit a_9 operate for preparing juice concentrate by means of evaporation. At this section necessary ingredients like sugar, preservatives, etc. are mixed in product. Here a perfect switching a_8 is also used between unit a_7a_9 to control the separation of processes. Now we pasteurize the products at unit a_{10} and forward to the packaging unit a_{11} where both the products are packed, as

ready to drink juice (RTD) packed in bottle and concentrate packed in cans and made ready to supply in market.

State configuration of juice plant under consideration is given below:



2. Assumptions or Notations

The determination of reliability of model described in this paper, using Boolean Function Technique, the following assumptions are (taken into account) made:

- (1) All the components/subsystems are in good and operable condition, initially.
- (2) The Failure times are arbitrary for all the components.
- (3) The state of all components is statistically independent.
- (4) In the system, each of the components is either in good or in failed state.
- (5) Reliability of every component or stage is known in advance.
- (6) The repair facility for any failed component is not available.
- (7) The whole system will fail if there is failure in any one of its units.

3. Mathematical Notations

a_1, a_2 : States of extraction unit	$\begin{bmatrix} a_2 & a_3 & a_6 & a_8 & a_9 \\ a_2 & a_4 & a_5 & a_6 & a_7 \\ a_2 & a_4 & a_5 & a_6 & a_8 & a_9 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \end{bmatrix}$
a_3, a_5 : States of storage tanks	$a_2 \ a_4 \ a_5 \ a_6 \ a_8 \ a_9$
a_{4},a_{8} : States of Perfect switching devices	where $L_1 = a_1 \ a_3 \ a_6 \ a_7 $
a_6 : State of Processing unit	$L_2 = a_1 \ a_3 \ a_6 \ a_8 \ a_9 $
a_7, a_9 : States of Production section	$L_3 = \begin{vmatrix} a_1 & a_4 & a_5 & a_6 & a_7 \end{vmatrix}$
a_{10} : State of Pasteurizing unit	$L_4 = \left \begin{array}{ccc} a_1 & a_4 & a_5 & a_6 & a_8 & a_9 \end{array} \right $
a_{11} : State of Packaging unit	
a_i : State of components which is equal to 1/0 in good/failed	$L_5 = \left \begin{array}{ccc} a_2 & a_3 & a_6 & a_7 \end{array} \right $
state $\forall i = 1, 2, 3,, 11$.	$L_6 = \left \begin{array}{ccc} a_2 & a_3 & a_6 & a_8 & a_9 \end{array} \right $
a_i' : Negation of a_i	$L_7 = ig egin{array}{cccccccccccccccccccccccccccccccccccc$
∧: Conjunction	$L_8 = a_2 \ a_4 \ a_5 \ a_6 \ a_8 \ a_9 $

||: Logical Matrix

 R_i : Reliability of ith component of the system.

 $Q_i: 1-R_i, \forall i = 1, 2, 3, \dots, 11$

 R_s : Reliability of the whole system.

 R_{SE}/R_{SW} : Reliability of ith component of the system.

4. Formulation of Mathematical Model

Incorporating Boolean Function Technique, The possible successful operating conditions of juice plant in terms of logical matrix are:

		$2, \ldots,$							
	a_1	<i>a</i> ₃	a_6	a_7	a_{10} a_{9} a_{7} a_{8} a_{10} a_{9} a_{7} a_{8}	a_{11}			
	a_1	a_3	a_6	a_8	a_9	a_{10}	a_{11}		
	a_1	a_4	a_5	a_6	a_7	a_{10}	a_{11}		
_	a_1	a_4	a_5	a_6	a_8	<i>a</i> 9	a_{10}	a_{11}	(4.1)
_	a_2	a_3	a_6	a_7	a_{10}	a_{11}			(4.1)
	a_2	a_3	a_6	a_8	a_9	a_{10}	a_{11}		
	a_2	a_4	a_5	a_6	a_7	a_{10}	a_{11}		
	a_2	a_4	a_5	a_6	a_8	a_9	a_{10}	a_{11}	

5. Solution of Model

By means of algebra of logics, Equation (4.1) can be expressed as:

$$F(a_1, a_2, \dots, a_{11}) = [a_{11} \wedge a_{10} \wedge f(a_1, a_2, a_3, \dots, a_{11})]$$
(5.1)

where $f(a_1, a_2, a_3, \dots, a_{11})$

$\begin{vmatrix} a_1 \\ a_1 \\ a_1 \\ a_1 \\ a_2 \\ a_2 \\ a_2 \\ a_2 \\ a_2 \end{vmatrix}$	$a_3 \\ a_3 \\ a_4 \\ a_4 \\ a_3 \\ a_3 \\ a_4 \\ a_4 \\ a_4$	$a_{6} \\ a_{6} \\ a_{5} \\ a_{5} \\ a_{6} \\ a_{6} \\ a_{5} \\ a_{5}$	a_7 a_8 a_6 a_7 a_8 a_6 a_6 a_6	a9 a7 a8 a9 a7 a8	<i>a</i> 9 <i>a</i> 9	=	$egin{array}{c} L_1 \ L_2 \ L_3 \ L_4 \ L_5 \ L_6 \ L_7 \ L_8 \end{array}$	(5.2)
a_2	a_4	a_5	a_6	a_8	<i>a</i> 9		L_8	
	$\begin{vmatrix} a_1\\a_1\\a_1\\a_1\\a_2\\a_2\\a_2\\a_2\\a_2\end{vmatrix}$	$\begin{vmatrix} a_1 & a_3 \\ a_1 & a_3 \\ a_1 & a_4 \\ a_1 & a_4 \\ a_2 & a_3 \\ a_2 & a_3 \\ a_2 & a_4 \\ a_2 & a_4 \end{vmatrix}$	$\begin{vmatrix} a_1 & a_3 & a_6 \\ a_1 & a_3 & a_6 \\ a_1 & a_4 & a_5 \\ a_1 & a_4 & a_5 \\ a_2 & a_3 & a_6 \\ a_2 & a_3 & a_6 \\ a_2 & a_4 & a_5 \\ a_2 & a_4 & a_5 \end{vmatrix}$	$ \begin{vmatrix} a_1 & a_3 & a_6 & a_7 \\ a_1 & a_3 & a_6 & a_8 \\ a_1 & a_4 & a_5 & a_6 \\ a_1 & a_4 & a_5 & a_6 \\ a_2 & a_3 & a_6 & a_7 \\ a_2 & a_3 & a_6 & a_8 \\ a_2 & a_4 & a_5 & a_6 \\ a_2 & a_4 & a_5 & a_6 \end{vmatrix} $	$ \begin{vmatrix} a_1 & a_3 & a_6 & a_7 \\ a_1 & a_3 & a_6 & a_8 & a_9 \\ a_1 & a_4 & a_5 & a_6 & a_7 \\ a_1 & a_4 & a_5 & a_6 & a_8 \\ a_2 & a_3 & a_6 & a_7 \\ a_2 & a_3 & a_6 & a_8 & a_9 \\ a_2 & a_4 & a_5 & a_6 & a_7 \\ a_2 & a_4 & a_5 & a_6 & a_8 \\ \end{vmatrix} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{vmatrix} a_1 & a_3 & a_6 & a_7 \\ a_1 & a_3 & a_6 & a_8 & a_9 \\ a_1 & a_4 & a_5 & a_6 & a_7 \\ a_1 & a_4 & a_5 & a_6 & a_8 & a_9 \\ a_2 & a_3 & a_6 & a_7 \\ a_2 & a_3 & a_6 & a_8 & a_9 \\ a_2 & a_4 & a_5 & a_6 & a_7 \\ a_2 & a_4 & a_5 & a_6 & a_8 & a_9 \end{vmatrix} = $	$\begin{vmatrix} a_1 & a_3 & a_6 & a_7 \\ a_1 & a_3 & a_6 & a_8 & a_9 \\ a_1 & a_4 & a_5 & a_6 & a_7 \\ a_2 & a_3 & a_6 & a_7 \\ a_2 & a_3 & a_6 & a_8 & a_9 \\ a_2 & a_4 & a_5 & a_6 & a_7 \\ a_2 & a_4 & a_5 & a_6 & a_7 \\ a_2 & a_4 & a_5 & a_6 & a_8 & a_9 \\ \end{vmatrix} = \begin{vmatrix} L_1 \\ L_2 \\ L_2 \\ L_3 \\ L_4 \\ L_5 \\ L_6 \\ L_7 \\ L_8 \end{vmatrix}$

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By orthogonalization algorithm, we may write (5.2) as

$$f(a_{1},a_{2},a_{3},\ldots,a_{11}) = \begin{vmatrix} L_{1} & & & \\ L'_{1} & L'_{2} & & & \\ L'_{1} & L'_{2} & L'_{3} & & & \\ L'_{1} & L'_{2} & L'_{3} & L'_{4} & L'_{5} & & \\ L'_{1} & L'_{2} & L'_{3} & L'_{4} & L'_{5} & L'_{6} & \\ L'_{1} & L'_{2} & L'_{3} & L'_{4} & L'_{5} & L'_{6} & L'_{7} & \\ L'_{1} & L'_{2} & L'_{3} & L'_{4} & L'_{5} & L'_{6} & L'_{7} & L_{8} \end{vmatrix}$$

$$(5.3)$$

Now $L_1 = \begin{vmatrix} a_1 & a_3 & a_6 & a_7 \end{vmatrix}$

$$L_{1}'L_{2} = \begin{vmatrix} a_{1}' & & \\ a_{1} & a_{3} & a_{6}' \\ a_{1} & a_{3} & a_{6} & a_{7} \end{vmatrix} \land \begin{vmatrix} a_{1} & a_{3} & a_{6} & a_{8} & a_{9} \end{vmatrix}$$

$$L_{1}'L_{2} = \begin{vmatrix} a_{1} & a_{3} & a_{6} & a_{7} \end{vmatrix} \land \begin{vmatrix} a_{1} & a_{3} & a_{6} & a_{8} & a_{9} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3} = \begin{vmatrix} a_{1} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3}'L_{4} = \begin{vmatrix} a_{1} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3}'L_{4} = \begin{vmatrix} a_{1} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3}'L_{4}'L_{5} = \begin{vmatrix} a_{1} & a_{2} & a_{3} & a_{6} & a_{7} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3}'L_{4}'L_{5}'L_{6} = \begin{vmatrix} a_{1}' & a_{2} & a_{3} & a_{6} & a_{7} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3}'L_{4}'L_{5}'L_{6}'L_{7} = \begin{vmatrix} a_{1}' & a_{2} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7} \end{vmatrix}$$

$$L_{1}'L_{2}'L_{3}'L_{4}'L_{5}'L_{6}'L_{7} = \begin{vmatrix} a_{1}' & a_{2}' & a_{3} & a_{4} & a_{5} & a_{6} & a_{8} & a_{9} \end{vmatrix}$$
Putting all in (5.3), we get

$$f(a_{1},a_{2},a_{3},\ldots,a_{11})$$

$$=\begin{vmatrix}a_{1}&a_{3}&a_{6}&a_{7}\\a_{1}&a_{3}&a_{6}&a_{7}\\a_{1}&a_{3}&a_{6}&a_{7}\\a_{1}&a_{3}'&a_{4}&a_{5}&a_{6}&a_{7}\\a_{1}&a_{2}'&a_{3}&a_{6}&a_{7}\\a_{1}'&a_{2}&a_{3}&a_{6}&a_{7}\\a_{1}'&a_{2}&a_{3}'&a_{4}&a_{5}&a_{6}&a_{7}\\a_{1}'&a_{2}&a_{3}'&a_{4}&a_{5}&a_{6}&a_{7}\\a_{1}'&a_{2}'&a_{3}'&a_{4}&a_{5}&a_{6}&a_{8}&a_{9}\end{vmatrix}$$
(5.4)

Therefore (5.1) becomes

$$f(a_{1},a_{2},a_{3},\ldots,a_{11})$$

$$= \begin{vmatrix} a_{1} & a_{3} & a_{6} & a_{7} & a_{10} & a_{11} \\ a_{1} & a_{3} & a_{6} & a_{7}' & a_{8} & a_{9} & a_{10} & a_{11} \\ a_{1} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7} & a_{10} & a_{11} \\ a_{1} & a_{2} & a_{3} & a_{6} & a_{7}' & a_{8} & a_{9} & a_{10} & a_{11} \\ a_{1} & a_{2} & a_{3} & a_{6} & a_{7}' & a_{8} & a_{9} & a_{10} & a_{11} \\ a_{1}' & a_{2} & a_{3} & a_{6} & a_{7}' & a_{8} & a_{9} & a_{10} & a_{11} \\ a_{1}' & a_{2} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7}' & a_{10} & a_{11} \\ a_{1}' & a_{2} & a_{3}' & a_{4} & a_{5} & a_{6} & a_{7}' & a_{10} & a_{11} \\ a_{1}' & a_{2}' & a_{3} & a_{4} & a_{5} & a_{6} & a_{8} & a_{9} & a_{10} & a_{11} \\ \end{pmatrix}$$

$$(5.6)$$

This equation is the disjoint of disjoint conjunctions; therefore we can calculate the reliability of whole system which is given by

$$R_S = P_r\{f(a_1, a_2, a_3, \dots, a_{11})\} = 1$$
(5.7)

or,

$$R_{S} = R_{10}R_{11}\{R_{1}R_{3}R_{6}R_{7} + R_{1}R_{3}R_{6}Q_{7}R_{8}R_{9} + R_{1}Q_{3}R_{4}R_{5}R_{6}R_{7} + R_{1}Q_{3}R_{4}R_{5}R_{6}Q_{7}R_{8}R_{9} + R_{1}R_{2}R_{3}R_{6}R_{7} + Q_{1}R_{2}R_{3}R_{6}Q_{7}R_{8}R_{9} + Q_{1}R_{2}Q_{3}R_{4}R_{5}R_{6}R_{7} + Q_{1}Q_{2}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}$$

$$(5.8)$$

where R_i is the reliability of *i*th state of the system and $Q_i = 1 - R_i$, $\forall i = 1, 2, 3, ..., 11$.

$$\begin{split} R_{S} &= R_{1}R_{3}R_{6}R_{7}R_{10}R_{11} + R_{1}R_{3}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{1}R_{3}R_{6}R_{7}R_{8}R_{9}R_{10}R_{11} + R_{1}R_{4}R_{5}R_{6}R_{7}R_{10}R_{11} \\ &- R_{1}R_{3}R_{4}R_{5}R_{6}R_{7}R_{10}R_{11} + R_{1}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{1}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} - R_{1}R_{4}R_{5}R_{6}R_{7}R_{8}R_{9}R_{10}R_{11} \\ &+ R_{1}R_{3}R_{4}R_{5}R_{6}R_{7}R_{8}R_{9}R_{10}R_{11} + R_{1}R_{2}R_{3}R_{6}R_{7}R_{10}R_{11} \\ &+ R_{2}R_{3}R_{6}R_{8}R_{9}R_{10}R_{11} - R_{1}R_{2}R_{3}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{2}R_{3}R_{6}R_{7}R_{8}R_{9}R_{10}R_{11} + R_{1}R_{2}R_{3}R_{6}R_{7}R_{8}R_{9}R_{10}R_{11} \\ &+ R_{2}R_{4}R_{5}R_{6}R_{7}R_{10}R_{11} - R_{1}R_{2}R_{4}R_{5}R_{6}R_{7}R_{10}R_{11} \\ &- R_{2}R_{3}R_{4}R_{5}R_{6}R_{7}R_{10}R_{11} - R_{1}R_{3}R_{4}R_{5}R_{6}R_{7}R_{10}R_{11} \\ &+ R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} - R_{1}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{2}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} - R_{1}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{2}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} + R_{1}R_{2}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{2}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_{11} + R_{1}R_{2}R_{3}R_{6}R_{8}R_{9}R_{10}R_{11} \\ &- R_{2}R_{3}R_{4}R_{5}R_{6}R_{8}R_{9}R_{10}R_$$

$$R_{S} = x_{1} + x_{2} - y_{1} + x_{3} - y_{2} + x_{4} - y_{3} - y_{4} + x_{5}$$

+ $x_{6} + x_{7} - y_{5} - y_{6} + x_{8} + x_{9} - y_{7} - y_{8} + x_{10}$
+ $x_{11} - y_{9} - y_{10} + x_{12}$ (5.9)

Case – (1) when reliability of each component is **R**, Then (5.9) gives:

$$R_S = 2R^6 + 3R^7 - 4R^8 - 2R^9 + 2R^{10}$$
(5.10)

Case - (5.1) when failure rates follow Weibull time distribution:

Let m_i is the rate of failure for *i*th state of system where i, j = 1, 2, 3, ..., 11, then reliability of system at any time "*t*", is calculated by

$$R_{SW}(t) = \sum_{i=1}^{12} \exp\{-x_i t^p\} - \sum_{j=1}^{10} \exp\{-y_j t^p\}$$
(5.11)

where *p* is a parameter (p > 0) and x_i, y_j , are given above

Case – (3) when failure rates follow Exponential time distribution:

Taking p = 1 in case (5.1), it will become Exponential time distribution, then we have

$$R_{SE}(t) = \sum_{i=1}^{12} \exp\{-x_i t\} - \sum_{j=1}^{10} \exp\{-y_j t\}, \dots, \quad (5.11)$$

Where x_i , y_j taken as in case (5.1).

In this case, the expression for another reliability parameter i.e. M.T.T.F. given by

$$M.T.T.F = \int_0^\infty R_{SE}(t)dt = \sum_{i=1}^{12} \left[\frac{1}{x_i}\right] - \sum_{j=1}^{10} \left[\frac{1}{y_j}\right]$$
(5.12)

6. Numerical Calculations

For Numerical computation, let us setting the values as:

- (1) $m_i = 0.001, t = 0, 1, 2, ..., p = 2$ in equation (5.11) where i = 1, 2, 3, ..., 11.
- (2) $m_i = 0.001, t = 0, 1, 2, ...$ in equation (5.11) where i = 1, 2, 3, ..., 11.
- (3) $m_i = 0.0, 0.1, 0.2, \dots, 1.0$ in equation (5.12) where $i = 1, 2, 3, \dots, 11$.

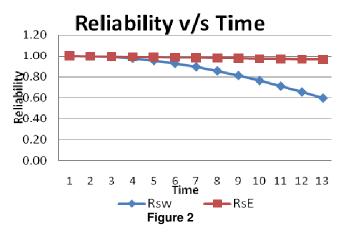
The computed results are given in Table 1 and Table 2 and graphically shown in Figure 2 and Figure 3 respectively.

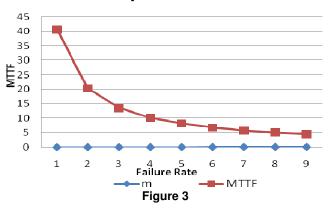
Table 4

Table 1					
Sr. No.	t	R _{SW}	R _{SE}		
1	0	1.000000000	1.000000000		
2	1	0.9970005075	0.9970005075		
3	2	0.9880084829	0.9940020602		
4	3	0.9730460385	0.9910047034		
5	4	0.9521593699	0.9880084829		
6	5	0.9254331315	0.9850134446		
7	6	0.8930106164	0.9820196345		
8	7	0.8551185369	0.9790270991		
9	8	0.8120937128	0.9760358849		
10	9	0.7644075017	0.9730460385		
11	10	0.7126828900	0.9700576069		
12	11	0.6576992298	0.9670706371		
13	12	0.6003808648	0.9640851762		

Та	hl	P	2	
10		C	~	

m	MTTF
0.01	40.6349206349
0.02	20.3174603175
0.03	13.5449735450
0.04	10.1587301587
0.05	8.1269841270
0.06	6.7724867725
0.07	5.8049886621
0.08	5.0793650794
0.09	4.5149911817
0.1	4.0634920635





MTTF v/s Failure Rate

7. Conclusion

The author has analyzed a **Juice Packaging Plant** for determining various reliability parameters by applying the Boolean Function Technique & algebra of logics.

In Table 1, Reliability of system is computed with respect to time when failure rates follow Weibull time distribution and exponential time distribution. The graph of "Reliability v/s Time" in the figure-2 depicts that the reliability of the complex system decreases approximately at a uniform rate in case of Exponential Time Distributions, but it decreases very rapidly, in case when failure rates follow Weibull Time Distributions.

In Table 2, MTTF is calculated and the graph "MTTF v/s Failure Rate" in figure-3 depicts that MTTF of the system decreases catastrophically in beginning but later it decreases approximately at a uniform rate.

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******** ISSN(P):2319-3786 Malaya Journal of Matematik ISSN(O):2321-5666 ********

